PHOTOGRAPHIC THREE-LENS OBJECTIVE

Filed July 10, 1931

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	s:
$r_{1} = + 24.2$ $r_{2} = -555.0$ $r_{3} = -96.0$ $r_{4} = + 24.0$ $r_{5} = -166.0$ $r_{7} = -45.2$ $r_{1} = -4.2$ $r_{1} = -4.2$ $r_{2} = -555.0$ $r_{3} = -24.0$ $r_{4} = -24.0$ $r_{5} = -24.0$ $r_{5} = -24.0$ $r_{7} = -45.2$	} 5 ? }
	? ! 5
Fig. 2 Kinds of glass: I II and III IV Fig. 1 $\begin{cases} n_d = 1.58315 & 1.58215 & 1.67110 \\ v = 59.3 & 42.0 & 47.3 \end{cases}$ I III III Fig. 2 $\begin{cases} n_d = 4.67110 & 1.62004 & 1.58215 \\ v = 47.3 & 36.3 & 42.0 & Inventor & 1.64004 \end{cases}$	

UNITED STATES PATENT OFFICE

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PHOTOGRAPHIC THREE-LENS OBJECTIVE

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those photographic three-lens objectivesi. e. spherically, astigmatically, comatically and chromatically corrected objectives which have a dispersing part enclosed with intermediate air spaces by two converging parts whereof one consists of two cemented members, namely a converging and a diverging member, and whereof both are of glass of at least a medial refractive index, that is to say of a refractive index of at least 1.55 approximately. The invention applies especially to such objectives in which the spherical correction is effected at least for a 13 medial aperture ratio, whereby for example the aperture ratio

$1:4\sqrt{2}(=1:5.657)$

of the English diaphragm scaling may be 20 considered as a medial aperture ratio, and whereby the diameter of the sharply defined image circle in the focal plane is approximately equal to the focal length. From the above it will be understood that universal objectives of great light transmitting capacity are concerned.

The invention provides objectives of the said kind which, with the usual extension of the field of view and with the usual image 30 quality, afford especially good images and, respectively, an especially great image field, when, according to its absolute value, the radius of the front refractive surface of the isolated dispersing lens is given relatively to the radius of the first refractive surface of the objective a ratio greater than 21/2, when, according to its absolute value, the radius of the last refractive surface of the objective is given relatively to the radius of the rear 40 refracting surface of the isolated dispersing lens a ratio greater than 134, and when care is taken that the last said ratio is always inferior to the first said ratio, and, in addition thereto, when the vertex distance of the first 45 part of the objective from the isolated diverging lens is inferior to 1½ times the vertex thickness of this lens. As a rule the aim of the invention is attained the more completely the smaller the value given the vertex dis-

The present invention aims at improving vertex distance even inferior to 11/3 times the vertex thickness of the isolated dispersing lens. Further, with a view to obtain a specially good correction, it is advisable to so arrange the converging part of two cemented 55 members that the convex side of the cemented surface faces the interior of the objective.

Two corresponding constructional examples are given in the annexed drawing as well as in the tables below. The radii, thick- 60 nesses and distances appearing therein are given in millimeters and refer to a focal length of the objective of 100 mm.

	First examp	le (Figure 1) " :	65
Radii		Thicknesses	Thicknesses and distances	
	$r_1 = +23.4$		= 4. 3	
	r ₂ == ∞	d_{11}	≈ 2.3	. •
	$r_1 = -81.3$ $r_4 = +22.4$		=4, 2	
	$\tau_4 = -322.0$		=1.3	
	$r_6 = +27.6$ $r_7 = -48.3$	diri :		70
		· · · · · · · · · · · · · · · · · · ·	- x. ;	
	Kinds	of glass		
Lens	. I	II=III	IV	
n_d $ u$	= 1. 58315 $=$ 59. 3	1, 58215 42, 0	1.67110 47.3	
Second example (Figure 2)				
	Radii	Thicknesses	and distances	
	$r_1 = + 24.2$		-4. 1	
	$r_3 = -555.0$ $r_3 = -96.0$		=2. 2 =3. 1	
	$r_4 = + 21.0$	b_1	=3.4	
	$r_b = -166.0$		≈2.6 0.7	80
	$r_4 = + 21.0$ $r_7 = -45.2$	div	=0.7 =4.4	
	-			
	Kinds of glass			
Lens	I=IV	II	III	
na	1.67110	1.62004	1. 58215	
v	47. 3	36. 3	42.0	85
TX71				

We claim:

1. A photographic objective, consisting of a dispersing part and two converging parts enclosing this dispersing part with inter-mediate air spaces, one of these converging 90 parts being composed of two cemented members whereof the one is converging and the other diverging, the two converging lenses of the objective being of glass of a refractive index of at least 1.55 approximately, the 95 radius of the front refractive surface of the isolated dispersing lens having relatively to the radius of the first refracting surface of the objective a ratio which, according to its ab-50 tance. Therefore it is advisable to make the solute value, is greater than 21/2, the radius 100 of the last refracting surface of the objective having relatively to the radius of the rear refracting surface of the isolated dispersing lens a ratio which, according to its absolute value, is greater than 1¾, this last mentioned ratio being inferior to the first mentioned one, and the vertex distance of the first lens of the objective from the isolated dispersing lens being inferior to 1½ times the vertex thickness of this lens.

2. In an objective according to claim 1, the said vertex distance being inferior to 11/3. times the vertex thickness of the isolated dis-

persing lens.

3. In an objective according to claim 1 the cemented surface of the converging part of two cemented members facing with its convex side of the interior of the objective.

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